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Estimating Production Functions Methodology Extensions

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UBC Economics 567

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Mistakes have been made

Control function estimators of production functions have repeatedly been used without fully thinking through the underlying model and assumptions

Colinearity of flexible inputs with each other

- Pointed out by Ackerberg, Caves, and Frazer (2015)
- 2 Lack of relevant instrument for flexible input
 - Pointed out by Gandhi, Navarro, and Rivers (2016)
- Heterogeneous markups are incompatible with the monotonicity assumption
 - Mistake in De Loecker and Warzynski (2012) (1337 citations), repeated in De Loecker, Eeckhout, and Unger (2020) (1268 citations)
 - Pointed out by Doraszelski and Jaumandreu (2019), Doraszelski and Jaumandreu (2021)

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Critiques and extensions

- Levinsohn and Petrin (2003): investment often zero, so use other inputs instead of investment to form control function
- Ackerberg, Caves, and Frazer (2015): control function often collinear with l_{it} for it not to be must be firm specific unobervables affecting l_{it} (but not investment / other input or else demand not invertible and cannot form control function)
- Gandhi, Navarro, and Rivers (2016): relax scalar unobservable in investment / other input demand
- Wooldridge (2009): more efficient joint estimation
- Maican (2006) and Doraszelski and Jaumandreu (2013): endogenous productivity

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Section 1

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Ackerberg, Caves, and Frazer (2015): contributions

- Document collinearity problem in OP and Levinsohn and Petrin (2003)
 - Need *l_{it}*, *f_{it}*(*k_{it}*, *i_{it}*) not collinear, i.e. something causes variation in *l*, but not *k*
- Propose alternative estimator
- Relates estimator to dynamic panel (Blundell and Bond, 2000) approach

^{0*}These slides are based on the working paper version Ackerberg, Caves, and Frazer (2006).

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Ackerberg, Caves, and Frazer (201)

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Collinearity in OP 1

• OP assume $i_{it} = I_t(k_{it}, \omega_{it})$

- Symmetry, parsimony suggest $I_{it} = L_t(k_{it}, \omega_{it})$
- Then $I_{it} = L_t(k_{it}, I_t^{-1}(k_{it}, i_{it})) = g_t(k_{it}, i_{it})$

$$y_{it} = \beta_l I_{it} + f_t(k_{it}, i_{it}) + \epsilon_{it}$$

 I_{it} collinear with $f_t(k_{it}, i_{it})$

- Worse in Levinsohn and Petrin (2003)
 - Uses other input *m*_{it} to form control function

 $y_{it} = \beta_l I_{it} + \beta_k k_{it} + \beta_m m_{it} + \omega_{it} + \epsilon_{it}$ $m_{it} = M_t (k_{it}, \omega_{it})$

- Even less reason to treat labor demand differently than other input demand
- Collinearity still problem with parametric input demand

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- Plausible models that do not solve collinearity
 - Input price data
 - Must include in control function to preserve scalar unobservable
 - Same logic above implies *m* and *l* are functions of both prices, so still collinear
 - Adjustmest costs in labor
 - Need to add I_{it-1} to control function
 - Change in timing assumptions
 - Measurement error in / (but not m)
 - Solves collinearity, but makes $\hat{\beta}_l$ inconsistent
- Potential model change that removes collinearity
 - Optimization error in *l* (but not *m*)
 - *m* chosen, *l* specific shock revealed, *l* chosen
 - OP only: I_{it} chosen at t 1/2, $I_{it} = L_t(\omega_{it-1/2}, k_{it})$, i_{it} chosen at t

Collinearity in OP 2

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Collinearity in OP

ACF estimator

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ACF estimator

- Idea: like capital, labor is harder to adjust than other inputs
- Model: I_{it} chosen at time t 1/2, m_{it} at time t

• Implies
$$m_t = M_t(k_{it}, l_{it}, \omega_{it})$$

• Estimation:

$$y_{it} = \underbrace{\beta_k k_{it} + \beta_l l_{it} + f_t(m_{it}, k_{it}, l_{it})}_{\equiv \Phi_t(m_{it}, k_{it}, l_{it})} + \epsilon_{it} \text{ gives}$$

$$\hat{\omega}_{it}(\beta_k,\beta_l) = \hat{\Phi}_{it} - \beta_k k_{it} - \beta_l I_{it}$$

2 Moments from timing and Markov process for ω_{it} assumptions:

$$\omega_{it} = \mathsf{E}[\omega_{it}|\omega_{it-1}] + \xi_{it}$$

- $E[\xi_{it}|k_{it}] = 0$ as in OP
- $E[\xi_{it}|I_{it-1}] = 0$ from new timing assumption
- $\hat{\zeta}_{it}(\beta_k, \beta_l)$ as residual from nonparametric regression of $\hat{\omega}_{it}$ on $\hat{\omega}_{it-1}$
- Can add moments based on $E[\epsilon_{it}|\mathcal{I}_{it}] = 0$

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Relation to dynamic panel estimators

- Both derive moment conditions from assumptions about timing and information set of firm
- Dealing with ω
 - Dynamic panel: AR(1) assumption allows quasi-differencing
 - Control function: makes ω estimable function of observables
- Dynamic panel allows fixed effects, does not make assumptions about input demand
- Control function allows more flexible process for ω_{it}

Simulations

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• DGPS:

- 1 Consistent with their model, but not LP
- 2 Consistent with both
- 3 Combination that consistent with neither
- Add measurement error to materials

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|--|
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production

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Simulation Results

TABLE I

MONTE CARLO RESULTS^a

| Meas. Error | ACF | | | | LP | | | |
|----------------|-------|------------|-------------|----------------|-------------|----------------|------------|-----------|
| | βι | | β_k | | β_l | | β_k | |
| | Coef. | Std. Dev. | Coef. | Std. Dev. | Coef. | Std. Dev. | Coef. | Std. Dev. |
| | L | DGP1—Seria | lly Correla | ted Wages an | d Labor Se | et at Time t – | - <i>b</i> | |
| 0.0 | 0.600 | 0.009 | 0.399 | 0.015 | 0.000 | 0.005 | 1.121 | 0.028 |
| 0.1 | 0.596 | 0.009 | 0.428 | 0.015 | 0.417 | 0.009 | 0.668 | 0.019 |
| 0.2 | 0.602 | 0.010 | 0.427 | 0.015 | 0.579 | 0.008 | 0.488 | 0.015 |
| 0.5 | 0.629 | 0.010 | 0.405 | 0.015 | 0.754 | 0.007 | 0.291 | 0.012 |
| | | L | OGP2—OL | otimization E | rror in Lat | por | | |
| 0.0 | 0.600 | 0.009 | 0.400 | 0.016 | 0.600 | 0.003 | 0.399 | 0.013 |
| 0.1 | 0.604 | 0.010 | 0.408 | 0.016 | 0.677 | 0.003 | 0.332 | 0.011 |
| 0.2 | 0.608 | 0.011 | 0.410 | 0.015 | 0.725 | 0.003 | 0.289 | 0.010 |
| 0.5 | 0.620 | 0.013 | 0.405 | 0.017 | 0.797 | 0.003 | 0.220 | 0.010 |
| | DG | P3—Optimiz | zation Erro | or in Labor a | nd Serially | Correlated W | Vages | |
| | | and La | bor Set at | Time $t - b$ (| DGP1 plus | DGP2) | 0 | |
| 0.0 | 0.596 | 0.006 | 0.406 | 0.014 | 0.473 | 0.003 | 0.588 | 0.016 |
| 0.1 | 0.598 | 0.006 | 0.422 | 0.013 | 0.543 | 0.004 | 0.522 | 0.014 |
| 0.2 | 0.601 | 0.006 | 0.428 | 0.012 | 0.592 | 0.004 | 0.473 | 0.012 |
| 0.5 | 0.609 | 0.007 | 0.431 | 0.013 | 0.677 | 0.005 | 0.386 | 0.012 |

^a1000 replications. True values of β_l and β_k are 0.6 and 0.4, respectively. Standard deviations reported are of parameter estimates across the 1000 replications.

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Section 2

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Gandhi, Navarro, and Rivers (2016)

- Show that control function method is not nonparametrically identified when there are flexible inputs
- Propose alternate estimate that uses data on input shares and information from firm's first order condtiion
- Show that value-added and gross output production functions are incompatible
- Application to Colombia and Chile

Assumptions

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1 Hicks neutral productivity $Y_{jt} = e^{\omega_{jt} + \epsilon_{jt}} F_t(L_{jt}, K_{jt}, M_{jt})$ 2 ω_{it} Markov, ϵ_{it} i.i.d.

- **3** K_{jt} and L_{jt} determined at t 1, M_{jt} determined flexibly at t
 - *K* and *L* play same role in the model, so after this slide I will drop *L*
- (4) $M_{jt} = \mathbb{M}_t(L_{jt}, K_{jt}, \omega_{jt})$, monotone in ω_{jt}

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Reduced form

• Let
$$h(\omega_{jt-1}) = E[\omega_{jt}|\omega_{jt-1}]$$
, $\eta_{jt} = \omega_{jt} - h(\omega_{jt-1})$
• log output

$$y_{jt} = f_t(k_{jt}, m_{jt}) + \omega_{jt} + \epsilon_{jt}$$

= $f_t(k_{jt}, m_{jt}) + \underbrace{h(\mathbb{M}_{t-1}^{-1}(k_{jt-1}, m_{jt-1}))}_{=h_{t-1}(k_{jt-1}, m_{jt-1})} + \eta_{jt} + \epsilon_{jt}$

• Assumptions imply

$$\mathbb{E}[\eta_{jt}|\underbrace{k_{jt}, k_{jt-1}, m_{jt-1}, \dots, k_{j1}, m_{j1}}_{=\Gamma_{jt}}] = 0$$

Reduced form

$$\mathsf{E}[y_{jt}|\Gamma_{jt}] = \mathsf{E}[f_t(k_{jt}, m_{jt})|\Gamma_{jt}] + h_{t-1}(k_{jt-1}, m_{jt-1})$$
(1)

• Identification: given observed $E[y_{jt}|\Gamma_{jt}]$ is there a unique f_t , h_{t-1} that satisfies (3)?

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Example: Cobb-Douglas 1

- Let $f_t(k,m) = \beta_k k + \beta_m m$
- Assume firm is takes prices as given
- First order condition for *m* gives

$$m = constant + rac{eta_k}{1 - eta_m}k + rac{1}{1 - eta_m}\omega$$

Put into reduced form

$$E[y_{jt}|\Gamma_{jt}] = C + \frac{\beta_k}{1 - \beta_m} k_{jt} + \frac{\beta_m}{1 - \beta_m} E[\omega_{jt}|\Gamma_{jt}] + h_{t-1}(k_{jt-1}, m_{jt-1})$$
(2)

• ω Markov and $\omega_{jt-1} = \mathbb{M}_{t-1}^{-1}(k_{jt-1}, m_{jt-1})$ implies

$$E[\omega_{jt}|\Gamma_{jt}] = E[\omega_{jt}|\omega_{jt-1}] = \mathbb{M}_{t-1}^{-1}(k_{jt-1}, m_{jt-1})] = h_{t-1}(k_{jt-1}, m_{jt-1})$$

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Example: Cobb-Douglas 2

• Which leaves

$$\Xi[y_{jt}|\Gamma_{jt}] = constant + \frac{\beta_k}{1 - \beta_m} k_{jt} + \frac{1}{1 - \beta_m} h_{t-1}(k_{jt-1}, m_{jt-1})$$
(3)

from which β_k , β_m are not identified

- Rank condition fails, $E[m_{jt}|\Gamma_{jt}]$ is colinear with $h_{t-1}(k_{jt-1}, m_{jt-1})$
- After conditioning on k_{jt}, k_{jt-1}, m_{jt-1}, only variation in m_{jt} is from η_{jt}, but this is uncorrelated with the instruments

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Identification from first order conditions 1

• Since *m* flexible, it satisfies a simple static first order condition,

$$\rho_t = p_t \frac{\partial F_t}{\partial M} \mathbb{E}[e^{\epsilon_{jt}}] e^{\omega_{jt}}$$

$$\log \rho_t = \log p_t + \log \frac{\partial F_t}{\partial M}(k_{jt}, m_{jt}) + \log \mathbb{E}[e^{\epsilon_{jt}}] + \omega_{jt}$$

- $\bullet\,$ Problem: prices often unobserved, endogenous ω
- Solution: difference from output equation to eliminate ω, rearrange so that it involves only the value of materials and the value of output (which are often observed)

$$\underbrace{s_{jt}}_{\equiv \log \frac{\rho_t M_{jt}}{\rho_t Y_{jt}}} = \log \underbrace{G_t(k_{jt}, m_{jt})}_{\equiv \left(M_t \frac{\partial F_t}{\partial M}\right)/F_t} + \log \underbrace{E[e^{\epsilon_{jt}}]}_{\mathcal{E}} - \epsilon_{jt}$$

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D = f =

Identification from first order conditions 2

- Identifies elasticity up to scale, $G_t \mathcal{E}$ and ϵ_{jt} which identifie \mathcal{E}
- Integrating,

$$\int_{m_0}^{m_{jt}} G_t(k_{jt}, m)/m = f_t(k_{jt}, m_{jt}) + c_t(k_{jt})$$

identifies f up to location

Output equation

$$y_{jt} = \int_{m_0}^{m_{jt}} \tilde{G}_t(k_{jt}, m)/m - c_t(k_{jt}) + \omega_{jt} + \epsilon_{jt}$$
$$-c_t(k_{jt}) + \omega_{jt} = \underbrace{y_{jt} - \int_{m_0}^{m_{jt}} \tilde{G}_t(k_{jt}, m)/m - \epsilon_{jt}}_{\equiv \mathcal{Y}_{jt}}$$

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Identification from first order conditions 3

where the things on the right have already been identified

• Identify *c*^{*t*} from

$$\mathcal{Y}_{jt} = -c_t(k_{jt}) + \tilde{h}_t(\mathcal{Y}_{jt-1}, k_{jt-1}) + \eta_{jt}$$

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• Value added:

$$VA_{jt} = p_t Y_{jt} - \rho_t M_{jt}$$

= $p_t F_t(K_{jt}, \mathbb{M}_t(K_{jt}, \omega_{jt}))e^{\omega_{jt} + \epsilon_{jt}} - \rho_t \mathbb{M}_t(K_{jt}, \omega_{jt})$

• Envelope theorem implies elasticity $_{e^{\omega}}^{Y} \approx \text{elasticity}_{e^{\omega}}^{VA} (1 - \frac{\rho_t M_{jt}}{p_t Y_{jt}})$

Problems

- Production Hicks-neutral productivity does not imply value-added Hicks-neutral productivity
- Ex-post shocks ϵ_{jt} not accounted for in approximation

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- Look at tables
- Value-added estimates imply much more productivity dispersion than gross (90-10) ratio of 4 vs 2

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